

Restorative Bio-Compatible Prosthetic Epoxy-Zeolite Composites: Strength and Resistance

Starokadomsky D^{1,2*}, Reshetnyk M^{2,3}, Starokadomska A⁴, Kokhtych L^{5,6}, Shulga S¹ and Moshkivska N¹



¹Chuiko Institute of Surface Chemistry, National Academy of Sciences (NAS) of Ukraina, Kiev, Ukraine

²Institute of Geochemistry and Mineralogy NAS, Kiev, Ukraine

³National Natural History Museum NAS, Kiev, Ukraine

⁴Institute of Fish Industry Ukrainian Academy of Agrarian Sciences (NAAN), Kiev, Ukraine

⁵Institute of Physics NAS, Kiev, Ukraina

⁶Sikorsky Kiev Politechnic Institute (KPI), Ukraine

***Corresponding author:** Starokadomsky D, Chuiko Institute of Surface Chemistry, National Academy of Sciences (NAS) of Ukraina, Institute of Geochemistry and Mineralogy NAS, Kiev, Ukraine

ARTICLE INFO

Received:  July 02, 2021

Published:  July 13, 2021

Citation: Starokadomsky D, Reshetnyk M, Starokadomska A, Kokhtych L, Shulga S, Moshkivska N: Restorative Bio-Compatible Prosthetic Epoxy-Zeolite Composites: Strength and Resistance. Biomed J Sci & Tech Res. 37(1)-2021. BJSTR. MS.ID.005959.

ABSTRACT

A study on the complex effect of the microdisperse fraction of zeolite (50 wt%) on the strength and stability of the polyepoxide composite. The results indicate the prospects of using zeolite to increase the compressive strength and Young's modulus, adhesion to steel, microhardness of composites. It is established that the filling significantly increases the resistance to abrasion, aggressive liquids (acetone and peroxide solutions), fire resistance.

Keywords: (3-6 words) Epoxy Composite; Zeolite; Copper Powder; Strength; Stability

Introduction

The injection of inorganic binders into the epoxy resin is a known method of obtaining coatings, adhesives, compounds and repair compositions. Epoxy compositions with building binders are used as the basis for the production of self-leveling floors, repair compositions and industrial compounds [1-22]. Attempts to use epoxy compounds for implantation and exo-prosthetics [7-9,23,24] have become popular recently. Epoxy glass and carbon plastics, as well as composites with biocompatible fillers, were able to compete with traditional metal and other (ceramic, wood) materials. In particular, due to porosity, nerves, oxones and body cells can grow through the surface of epoxy materials (which is impossible for tantalum and titanium implants) [23,24]. And in exo-prosthetics (manufacturing of external prostheses), epoxy composites have a number of advantages - in particular, the possibility of manufacturing in the field, replaceability, ease [8,9,23,24]. An

interesting potential filler for biocompatible innovative epoxy composites is zeolite and its varieties. There are researches on the effect on epoxy polymers of montmorillonite [14,15,25], clays and brick dust [3,16], aluminum oxide [10,20,21], pyrophyllite [11], brick powders [3,16], natural zeolites [18], bentonite [22], copper [26,27]. These issues are dealt with by teams led by Danchenko & Barabash [19-21], Erdogan [18], Choi & Lee [15], Burmistrov & Mostovoy [16], Starokadomsky [3,10], Borisov and others [25], Kahramanov & Allahverdieva [26,27]. The aim of the work was to establish the possibilities of zeolite as a potentially enhancing eco- The Composites Department in Chuiko ISC has 30 years of experience in polymer research with alumina and silica, as evidenced by our works [1-13,19]. Also, we have experience in the creation of prosthetic [5,8,9] and biocompatible [7,11-13] compounds and fiberglass compatible and cheaper epoxy filler. The selected concentration of 50 wt% is practically convenient because

it forms a convenient viscous composition, and also allows you to mix components without precision scales (which is important in the field conditions). At the same time, epoxy-ceolite-copper composite was investigated in order to further create electro- and thermally conductive materials for electronics and medicine (prosthetics).

Figure 1 Pilot, Hero of the Soviet Union A. Maresyev (non-colored photos), in 1943-1946, on a military plane, flew 86 sorties with prostheses instead of amputated legs. Colored photo - examples of modern prostheses (see [28,29] and Wikipedia.org). Prosthetics has a long history. Even medieval Caribbean pirates also often had wooden legs and iron hooks instead of hands and fingers, and there have been attempts at dental prosthetics since primitive

times. However, real shifts in science and practice began in the last century. Already in the 2nd World War, there are vivid examples of the effectiveness of prosthetics for maintaining extreme loads. So, the Soviet pilot A. Maresyev (Figure 1), after being wounded and amputated of his legs, returned to the sky and flew with prostheses. In total, during the war, he made 86 sorties, shot down 10 enemy (german) aircraft: three before being wounded and seven after. A. Maresyev (1916-2001) lost his legs at the age of 37, but with prostheses he lived an active life for another 59 years, and died almost at 90 years old in the new XXI-th century. He became the prototype for the hero of the soviet bestseller "The Story of a Real Man" [28,29].



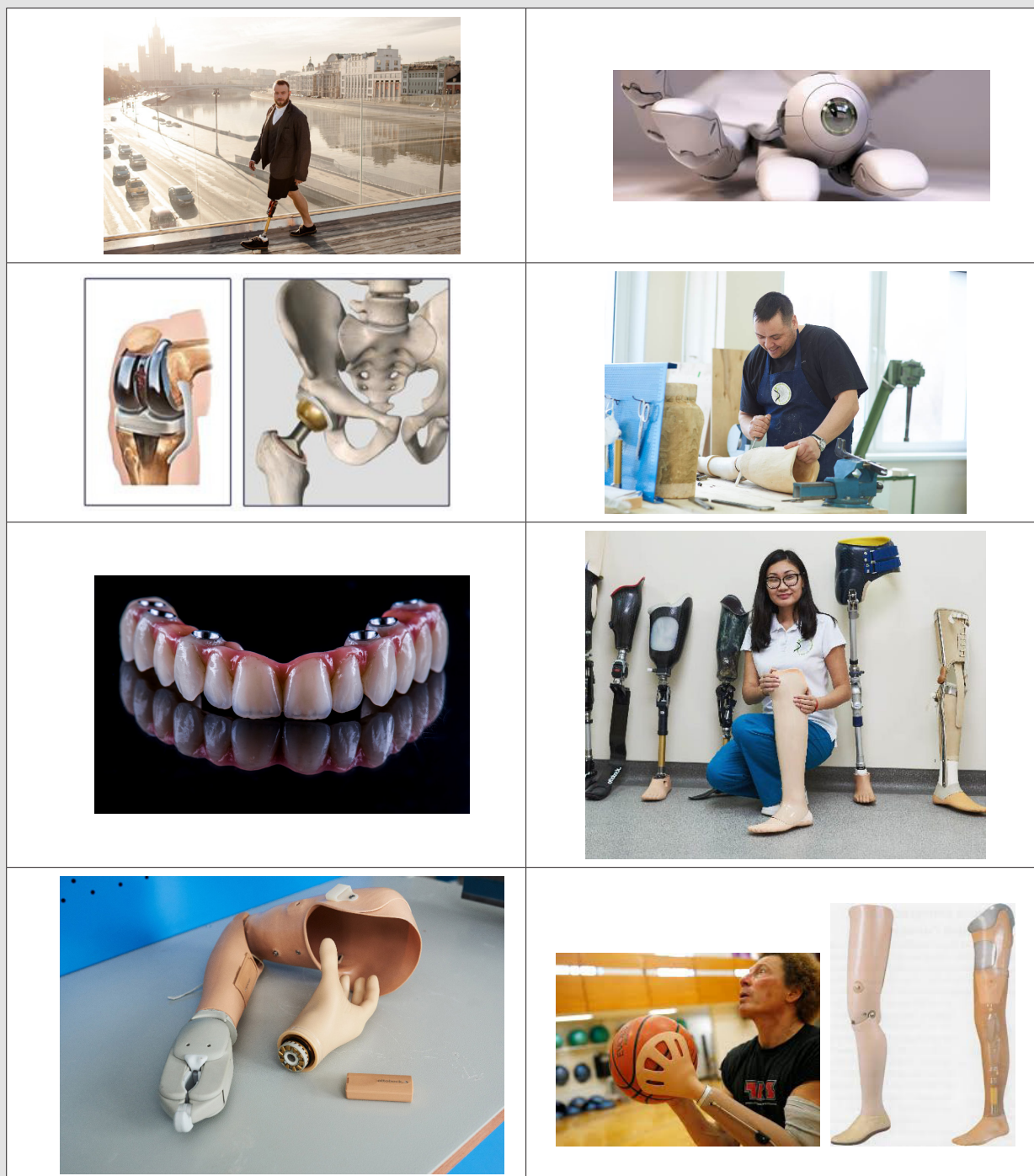


Figure 1: Pilot, Hero of the Soviet Union A. Maresyev (non-colored photos), in 1943-1946, on a military plane, flew 86 sorties with prostheses instead of amputated legs. Colored photo - examples of modern prostheses (see [28-29] and Wikipedia.org).

Methods and Reagents

Required Reagents and Method of Obtaining Composites

The Czech cold-hardening epoxy resin “Epoxy520” (Figure 2) was used for the works, which was cured with PEPA polyamine in a ratio of 5:1. The filler was added immediately after mixing these components, after which the composition was homogenized and

immediately formed into samples (Figure 3, Table1). As a filler were used nano- and micro-sized zeolite particles (manufactured by PE “Eco Instinct”) for which sieving up to 100 μm was performed. Its supramolecular structure provides for the presence of micropores and internal nanopores (Figure 4). Visually, it is a gray powder converting the epoxy composition to a viscous ochre mass (Figure 4). Curing them gives wood-like biocompatible composites (Figure

5). Of the strength properties, we were interested in those that practically determine the applicability of these compositions. These are adhesion, strength (and modulus of elasticity) in compression, bending and abrasion, microhardness. Determination of strength and stability was performed according to methods corresponding to standards (GOST or ASTM). Shear adhesion tests (GOST 14760-59) were performed on steel tear plates with a bonding area of 3cm² and are presented in kgf. The corresponding value of adhesive strength can be obtained by dividing the obtained index by three. For compression tests (taking into account GOST 4651-2014; ISO 604: 2002), cylindrical samples (diameter d= 6.5mm, height h=12 +1mm) were taken and compressed on a Louis Shopper press machine until complete destruction. The machine provided compression of the sample with a given constant speed of

movement of the active gripper, measurement of the load with an error of no more than $\pm 5\%$ of the measured value. According to the test results, the strength was calculated: $f = P / s$ (P - load in kgf, s - area equal to 0.332cm^2) and module E : $E = f / e$ (e - elongation equal to the length of the rectilinear section of the diagram in cm, divided by 10). Abrasion was performed by passing composite cylinders (diameter 6.5cm) on the surface of emery P60 at a distance of 10cm in both directions 40 times. Weight loss in mg and mm was determined. Abrasion resistance was calculated as the inverse of the abrasion mass of the sample. Abrasion resistance was determined by the empirical (derived from experiments) formula $W = 1 \times (m / mH) / P = m / mH \times P$, where mH / m characterizes the increase in mass (density) of the sample after filling.

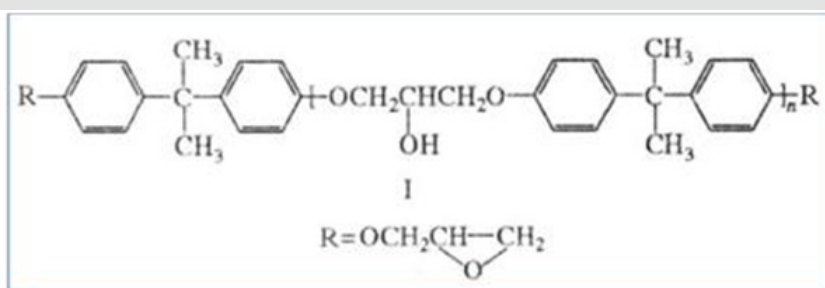


Figure 2: Epoxy-resin, typical shape and formula.

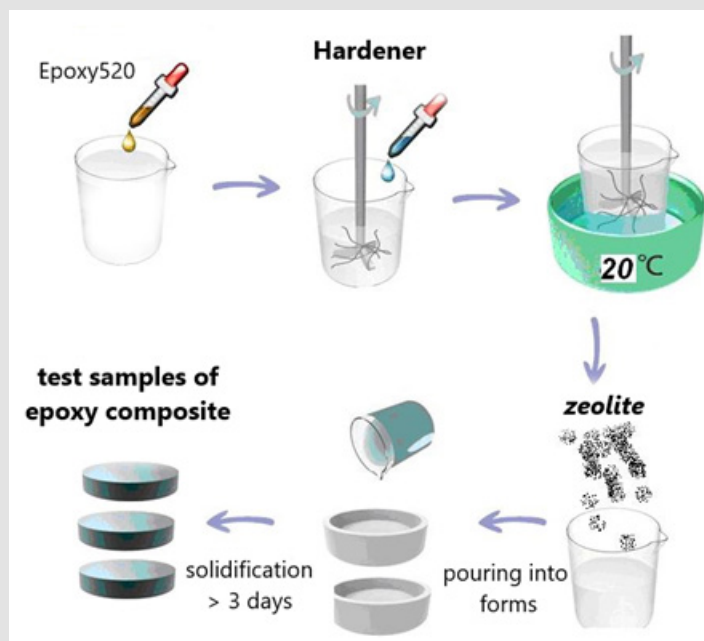


Figure 3: A typical scheme for obtaining epoxy-filled composites.

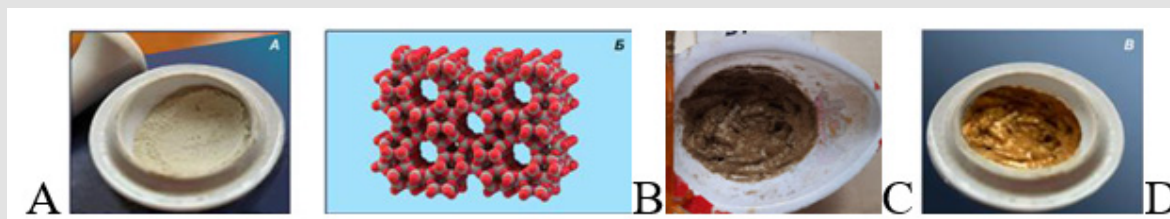


Figure 4: View of zeolite powder (A), zeolite structure (B), epoxy-zeolite (C) & epoxy-zeolite-Cu and (D) compositions

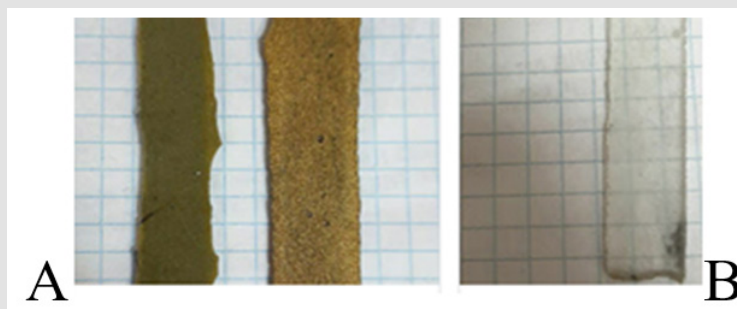


Figure 5: View of polymerized composites - epoxy-zeolite & epoxy-zeolite-Cu with (A) and without zeolite (B)

Table 1: Description and marking of samples.

Sample	Description
H (unfilled polymer)	Unfilled polymer
Z50%	Polymer with 50 wt% zeolite
Z50%+Cu	Polymer with 50 wt% zeolite and the addition of copper powder (15-20%)

Strength of Composite Materials

Adhesion Strength of the Epoxy-Composite to Steel

Shear adhesion to steel tends to be enhanced after the addition of 50% by weight of the zeolite. This can be seen from Table 2, from the results of which the most informative are the maximum obtained values (Table 2 d) and the modified average value (not taking into account the smallest indicators out of the series - in this case a) for C50%).

Table 2: Load values when testing adhesion to steel (bonded area 3 cm²).

Shear Adhesion, kgf		
	H	Z50%
a)	34	22
b)	35	30
c)	41	38
d)	42	51
Average value	38	35
Modif. average	38	40

Mechanical Abrasion of the Epoxy Composites

As can see (Table 3), the injection of fillers leads to a marked increase in abrasion resistance. This is also noticeable while

estimating abrasion in millimeters: the filled samples lose much less in size than the H-polymer sample. The increase in abrasion resistance (especially after the addition of copper, table 3) is quite natural, given the abrasive resistance of inorganic filler particles. Here need to notice also that the density of the sample naturally increases, especially after the addition of copper - even more (see the masses of the samples, Table 3).

Table 3: Abrasion of samples (emery P60, 40 passes in both directions on 10cm).

	H	Z50%	Z50%+Cu
The mass of the sample d=11mm	37	44	55
P, mg	8,5	7	7
L, mm	2,5	1,5	1,3
Abrasion resistance W=m/mH×P	0.12	0.17	0.21

Compressive Strength and Young Modulus of Composites

Table 4 demonstrate that 50 wt% zeolite makes it possible to increase the compressive strength and Young's modulus. When copper powder is added to the composition, the effect is enhanced - in particular, the maximum value obtained is increased by 20% (425 instead of 380) compared to the H-polymer. The filling also changes the nature of the destruction from plastic (the sample crumples

like plasticine) to brittle (cracks along the puncture lines). We can notice from Table 5, that process of filling gives approximately double growth of microhardness. However, the filling increases the fragility of the samples - they crack already when hemisphere-punch immersing to 20µm (Table 5) – while unfilled withstanding immersion up to 60µm. From the summary Table 6 you can see the overall effect of zeolite on the mechanical parameters of polyepoxide.

Table 4: Values of load F in compression (cylindrical specimens with a diameter d=6.5cm, height 11-12cm), Young's modulus E (*estimated) and the nature of the destruction of cracks when gripping.

	F, all values, kgf	F aver, kgf	E* MPa	Nature of Destruction
H	350 – 350 – 380 – 380	365	1,1	Plastic
Z50%	380 – 380 – 390 – 390	385	1,3	Fragile
Z50%+Cu	380 – 380 – 425	395	1,4	Fragile

Table 5: Microhardness (in H) of the surface of the composites, when the hemisphere is immersed by 10-30 microns. The # symbol indicates brittle cracking of the sample at the time of testing.

	10 mc	20 mc	30 mc
H	100	300	450
Z50%	200	400 #	
Z50%+Cu	200	400 #	

Table 6: All investigated parameters of strength of composites (* - aver (max) means Average and Maximal obtained value; ** - cylinder at h = 11mm, d = 6,5mm; *** - at 10 and 20µm immersion of steel hemisphere).

	H	Z50%	Z50%+Cu
Compression load F (kgf):*aver (max)	375 (380)	385 (395)	395 (425)
Modulus E ^F , ×10 ³ .kgf/cm ²	≈ 11	≈ 13	≈ 14
Sample weight, mg**	38	47	55
Shrinkage, mm	1,5	1	1
Abrasion, mg (mm)	7,5 (2,5)	7 (1,5)	7 (1,5)
Microhardness***, N	100 & 200	300 & 400	300 & 400
Fire resistance, sec	1	2	2
Adhesion, aver (max),kgf	38 (42)	40 (51)	-

Resistance and Swelling of the Epoxy Composite in Aggressive Environments

Endurance in 60% H₂O₂: Hydrogen peroxide, even at low concentrations (2-5%) is a substance quite aggressive against polymers (which is why it is used as a bleach in cosmetics). When the concentration of H₂O₂ reaches 30-40% and especially 50-60%, its destructive effect is multiplied. At concentrations of 50-60% peroxide easily corrodes organic tissues (in particular, forms severe burns on the skin). Polyepoxides are not significantly stable in 50-60% hydrogen peroxide. Therefore, the dynamics of their swelling and destruction in it can be tracked quite quickly (within 1-2 weeks) - in contrast to many other aggressive substances (acids, gasoline, alkalis). This makes the peroxide a convenient medium for evaluating the effect of the filling on the stability of the composite. From Table 7 it can be seen that the zeolite gives the composite greater resistance to peroxide. This can be seen from the decrease

From Table 6 it is seen that the introduction of 50 wt% zeolite makes it possible to increase the strength and Young's modulus under compression, microhardness, adhesion and fire resistance. This reduces shrinkage (an undesirable component of polymer synthesis) and abrasion wear. The addition of micro-nanoparticles of copper sometimes enhances the effect of increasing strength (for example, in compression).

in the degree of swelling at all stages of exposure. The addition of copper powder in the composition somewhat weakens the positive effect of the filling, bringing the swelling index to that for the unfilled (H) sample (Table 7, Figure 6).

Resistance in a Mixture of Acetone: Ethylacetate (1 : 1): Acetone and acetone-contained solvents are very aggressive media for polyepoxides [3-9]. The unfilled polymer (especially freshly made) destructs in acetone solvents in a matter of days and sometimes hours. At the same time, the filling of epoxides can significantly increase their resistance to these mediums [3-11]. This can be seen from the results obtained. The unfilled sample is strongly swollen already in the first hours of endurance, and at the end of 1 day of endurance completely destroys (scatters in solvent). After the introduction of zeolite, the charge does not destroy, and swells much more slowly than the H-polymer. The addition of copper powder enhances this effect (Table 8).

Water Absorption of Composites: Polyepoxides are generally quite stable in water. A water absorption rate of up to 1-2% during the month of exposure is considered normal. However, often even this figure needs to be improved. In addition. Epoxy products (coatings, parts, structures or ships) are often in the water for many years, and they need high water resistance. From our research we

can conclude that the addition of zeolite makes the composite somewhat more resistant to water in the first half of the exposure (Table 9). Filling even causes the effect of slight weight loss, which can be caused by the phenomena of leaching of substances from the structure of the zeolite filler.

Table 7: The degree of swelling of the samples in 60% H₂O₂.

Time, (in days)	H	Z50%	Z50%+Cu
0	0,0	0,0	0,0
0,04	1,5	1,7	3,5
1	2,0	2,3	4,7
2	3,5	1,7	4,1
3	4,5	2,9	3,5
5	4,5	2,9	3,5
12	5,1	4,0	4,7

Table 8: Swelling degree of samples in acetone: ethylacetate mixture.

Time, (in days)	H	Z50%	ZCu50%
0	0,0	0,0	0,0
0,03	6,7	2,2	1,1
0,05	7,9	3,1	0,5
0,08	12,1	2,6	1,6
1	destroys	12,7	9,3
2		17,5	12,0
4		17,9	15,3
5		18,8	15,3
8		20,1	18,6
12		21,4	18,6

Table 9: The degree of swelling of the samples in H₂O.

Time, (in days)	H	Z50%
0	0,0	0,0
0,04	1,7	1,1
1	1,3	-2,3
2	1,7	-1,5
4	1,7	-1,1
5	0,4	-1,1
12	2,6	-1,1
15	2,8	-1,1

Thermo-Oxidative Destruction of Polymer Powders without and with Filler

A significant increase in fire resistance (Table 6) gives reason to expect certain changes in resistance to destructive thermal oxidation (DTO). A typical thermogram of unfilled polyepoxide is presented in Figure 9H. It shows that the maximum weight loss due to destructive thermal oxidation (DTO) occurs at 300 oC. The temperature of the 5% weight loss of the H-polymer, respectively, is

275 oC, and 10% 300 oC (Figure 9H. TG curve). After that, the DTO processes are significantly slowed down, forming a cycle of primary destruction processes. Starting from 450 oC, secondary processes (called burnout of coke residue) are activated. They also have their peak activity but occur with a more active and stable (without sharp differences) dynamics of heat release and weight loss (Figure 9). Half (50%) of weight loss occurs at 525 oC. Secondary DTO processes are completed only at the approach of 800 oC, when almost 100%

of the sample burns out (Figure 9H). With the injection of 50 wt% zeolite, you can expect some changes in the thermal oxidation of the sample. Indeed, the primary DTO is less active. Thus, on the DTG curve at least at -0.1 (whereas for H-polymer at -0.2) and the DTA curve does not rise above 0.8. The maximum of the primary DTO is shifted toward 290 oC, ie at a lower temperature than the DTO of the H-polymer. Also, at lower temperatures (than for H-polymer) there is a secondary DTO, which according to the DTG curve is completed much faster - at 670 oC (H-polymer at 780 oC). At the

same time, only up to 60% of the sample burns out, obviously it is 50% of the polymer and another 10% of the zeolite mass. When adding 10-13 wt.% Micro nano-particles of copper in the composite with zeolite, the nature of the thermal decomposition changes markedly. Now we actually have a single DTO process that is made up of sequential processes. All destructive processes are completed in record time - up to 630 oC. From Figure 9 and Table 10 it is seen that the filling generally impairs the resistance of polyepoxide to thermal oxidative destruction.

Table 10: Stat-parameters of DTO processes, according to the obtained thermograms.

	H	Z50%	Z50%+Cu
To 10% loss weighth	300	290	290
To 5% loss weighth	275	275	250
To 50% loss weighth	525	580	580
To 50% loss weighth of destructed phase	525	450	410
To active loss weighth start	270	270	270
To end of loss weighth	800	660	640
Total loss weighth, %	98	58	53
1-th peak of DTG	300	290	≈275
2-th peak of DTG	575	550	≈500
Peak of DTA	600	500	480

Conclusion

- 1) The injection of zeolite (in the amount of 50 wt%) is promising for the production of bio-eco-compatible composites for industrial and biomedical use, with enhanced strength and stability characteristics. The addition of micro-nanoparticles of copper in the composition in some cases can enhance the quality and strengthening effects of polymerized composites.
- 2) It is experimentally shown that the introduction of zeolite can dramatically increase the stability in an aggressive solvent (a mixture of acetone: ethyl acetate). Unlike unfilled (which completely destroys in 1 day of endurance), composites don't destroy in it, and swell much more slowly. Also, the filling (after 2-3 days of exposure) increases the resistance to swelling in highly concentrated (60%) H₂O₂ peroxide: after 5 days of exposure, the unfilled swells by almost 5%, while the composite with zeolite - less than 3%.
- 3) It is established that the zeolite filling gives a double increase in microhardness and a slight increase in compressive strength and modulus. The addition of micro-nanoparticles of copper sometimes enhances the effect of increasing strength (for example, in compression). However, the filling increases the fragility of the samples.
- 4) It is shown that the filling doubles the fire resistance (2sec, whereas unfilled - 1sec). Thermogravimetry shows that

the filling does not increase the resistance to primary thermo-oxidation of the epoxy polymer (passes at 290 oC instead of 300 oC in the unfilled) but makes it less active. Also, at lower temperatures are the processes of secondary thermal oxidation (at 670 oC instead of 780 oC in the H-polymer). The positive effect of the filler is reflected in an almost twofold reduction in the burn-up mass (up to 50-60% of the sample instead of 98% in the unfilled one).

References

1. M Reshetnyk, D Starokadomsky, A Ishenko (2017) Filling with the Graphene Nanoplates as a Way to Improve Properties of Epoxy-Composites for Industrial and Geophysical Machinery. American Journal of Physics and Applications 5(6): 120-125.
2. Ary Subagia I, Tijing L, Kim Y (2014) Mechanical performance of multiscale basalt fiber-epoxy laminates containing tourmaline micro/nano particles. Composites (B: Engineering) 58: 611-617.
3. DL Starokadomsky (2012) About Possibilities of Strengthening of Epoxy polymer Composites by Modified Brick Powder. American Journal of Polymer Science 2(6): 109-114.
4. D Starokadomsky (2018) Long life of epoxy. Science and Life 1: 66-71.
5. D Rassokhin, D Starokadomsky, A Ishchenko, O Tkachenko, M Reshetnyk (2020) Determining the Strength and Thermal, Chemical Resistance of the Epoxy Polymer Composite Filled with Basalt Micro Nano Fiber in the Amount of 15–80% by Weight. Eastern-European Journal of Enterprise Technologies 2(104): 66-71.
6. D Starokadomsky, A Ishchenko, D Rassokhin, M Reshetnyk (2019) Epoxy composites for equipment repair with 50 wt% silicon carbide, titanium nitride, cement, gypsum: heat hardening effects, strength, resistance, morphology. Composites and Nanostuctures 2(42): 85-93.

7. Starokadomsky D, Halysh V, A Starokadomska, A Nikolaychuk, S Shulga, et al. (2020) Restorative biocompatible polymer composites on the base of epoxy-resin filled by surface-modified disperse utilized solid waste of industrial paper products. *Journal of Applied Surfaces and Interfaces* 8(1-3): 1-6.
8. D Starokadomsky, M Reshetnyk (2019) Microfilled Epoxy-Composites, Capable of Thermo-Hardening and Thermo-Plasticization After Hard Heating (200-300 OC)-For "in-Field\Offroad" Use in Bio-, Agro-, Medservice. *Biomedical Journal of Scientific and Technical Research* 19(1): 14118-14123.
9. Starokadomsky D, Reshetnyk M (2019) Epoxy Composites Reinforced with Bazaltfibre for Osteo-, Paleo-Prostheses and External Implants. *Biomedical Journal of Scientific and Technical Research* 18(1): 13237-13241.
10. Starokadomsky DL, Mishchenko VN (2012) Modified silica and alumina nanoparticles. Influence on strength and chemical resistance of polyepoxides filled with them. *Chemical Industry of Ukraine* 35: 41-46.
11. DL Starokadomsky, EM Pakhlov (2015) Physical and Mechanical Properties of Epoxy Composites With 10-50 wt% Pyrophyllite. *Composites and Nanostructures* 22(1): 41-51.
12. Starokadomskii D, Soloveva T (2002) Effect of silicon oxide fillers on photochemical curing of compounds based on acrylic monomers and oligomers. *Russian Journal of Applied Chemistry* 75: 138-141.
13. DL Starokadomsky (2008) About influence of non-modified nanosilica on physico-chemical properties of epoxy-polymer composites. *Russian Journal of Applied Chemistry* 12: 2045-2051.
14. Suy Yu, Seun Yang, Maen Cho (2009) Multi scale modeling of cross-linked epoxy composites. *Polymer* 50(3): 945-952.
15. YY Choi, SH Lee, SH Ryu (2009) Effect of silane functionalization of montmorillonite on epoxy/montmorillonite nanocomposite. *Polym Bull* 63: 47-55.
16. Mostovoi AS, Kurbatova EA (2017) Controlling the Properties of Epoxy Composites Filled with Brick Dust. *Russ J Appl Chem* 90(2): 267-276.
17. Burmistrov IN, Mostovoi AS, Shatrova NV, Panova LG, Kuznetsov DV, et al. (2013) Influence of Surface Modification of Potassium Polytitanates on the Mechanical Properties of Polymer Composites Thereof. *Russ J Appl Chem* 86(5): 765-771.
18. B Erdogan, AT Seyhan, Y Ocak, M Tanoğlu, D Balköse, et al. (2008) Cure Kinetics of Epoxy-Natural Ceolites Composites. *J Thermal Analysis & Calorimetry* 94: 743-750.
19. O Polovina, B Gorelov, A Gorb, A Nadtochiy, D Starokadomsky, et al. (2019) Epoxy filled with bare and oxidized multi-layered graphene nanoplatelets: a comparative study of filler loading impact on thermal properties. *Journal of Materials Science* 54(12): 9247-9266.
20. Y Danchenko, M Kachomanova, Y Barabash (2018) The acid-base interaction role in the processes of the filled diene epoxy resin structuring. *Chemistry & Chemical Technology* 12(2): 188-195.
21. E Barabash, Yu Popov, Yu Danchenko (2015) The influence of modifying additives on the adhesion of epoxyamine compositions (binders) to aluminoborosilicate glass and steel. *Science Newsletter of Budivnistva*, pp. 122-128.
22. V Osipchik, R Yakovleva, Y Danchenko, M Kachomanova, R Bykov (2007) Investigation of the effect of the surface properties of bentonite on the curing of epoxyamine compositions. *Advances in chemistry and chemical technology* 21(6): 74.
23. E Salernitano, C Migliaresi (2003) Composite Materials for Biomedical Applications: A Review *Journal of applied biomaterials & biomechanics (JABB)* 1(1): 3-18.
24. (2018) Master Bond EP42HT-2Med. Epoxy use in prosthetics and medical devices. *Today's Medical* - 4.
25. VA Borisov, A Yu Bedanokov, AM Karmokov, AK Mikitaev, MA Mikitaev, et al. (2007) Properties of polymer nanocomposites based on organomodified Na + -montmorillonite. *Plasticheskiye Massy* No 7: S30-32.
26. Kahramanov N, Bayramova I, Allahverdieva H, Namazly U, Pesetsky S (2020) Properties and Thermal Characteristics of Nanocomposites and Their Vulcanizes Based on A Copolymer of Ethylene with Butylene and Natural Minerals. *Composites and Nanostructures* 12(3): 107-113.
27. Allahverdieva H, Kahramanov N, Arzumano N, Abdalova S (2021) Thermo deformation Properties of Metal-Polymer Composites Based on Low Density Polyethylene and Copper. *Material ovedenie (Materials Science, in Russian)* 5: 36-40.
28. O Orlova (2021) History of prostheses.
29. (1948) Tale about the real man.

ISSN: 2574-1241

DOI: 10.26717/BJSTR.2021.37.005959

Starokadomsky D. Biomed J Sci & Tech Res



This work is licensed under Creative Commons Attribution 4.0 License

Submission Link: <https://biomedres.us/submit-manuscript.php>



Assets of Publishing with us

- Global archiving of articles
- Immediate, unrestricted online access
- Rigorous Peer Review Process
- Authors Retain Copyrights
- Unique DOI for all articles

<https://biomedres.us/>