

Mercurimetric Titration of Chloride in Presence of Sodium Nitroprusside as Indicator

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ABSTRACT

The mercurimetric titration of chloride with sodium nitroprusside used as indicator, is formulated. A systematic error involved, with location of the end point of titration is calculated at different concentrations of components in the system tested. The results of calculations, obtained with use of a computer program, are presented graphically.

Keywords: Chloride determination; Mercurimetric titration; Sodium nitroprusside; Systematic error

Introduction

A titration procedure aims to determine the concentration of a solute in a solution tested, in presence of an indicator used for registration of the end point (e) of the titration. For example, Cl^- ions are determined in Mohr's method by titration with AgNO_3 standard solution, in presence of K_2CrO_4 in the titrand [1-3]; the end point is indicated here by the Ag_2CrO_4 precipitate. In the Liebig method of cyanide determination, KCN solution is titrated with AgNO_3 solution; the end point is indicated here by AgCN precipitate [4,5], as auto-indicating species. In the Denigès' modification of the Liebig titration, the solution of $\text{KCN} + \text{KI} + \text{NH}_3$ is titrated with AgNO_3 solution; the end point is indicated here by the AgI precipitate [4,6]. Systematic error of the analyses was evaluated from calculations made on the basis of charge and concentration balances, and all thermodynamic knowledge expressed by equilibrium constants for the species related to the systems in question.

The present paper gives an evaluation of systematic error in mercurimetric titration of chloride in presence of sodium nitroprusside $\text{Na}_2\text{Fe}(\text{CN})_5\text{NO}\cdot 2\text{H}_2\text{O}$ as indicator [7-10]. The nitroprusside ions, $\text{Fe}(\text{CN})_5\text{NO}^{2-}$, form a white precipitate of $\text{HgFe}(\text{CN})_5\text{NO}$ [11,12]. The titration is performed at $\text{pH} = 1.5 - 2$ [13].

Here and in further parts of this paper, the charges z_i of the corresponding species $X_i^{z_i}$ ($i=1,2,\dots$) are omitted, when written in

terms of molar concentrations, i.e., the notation $[X_i]$ is applied here, for simplicity.

Some preliminary remarks

The system considered is an example of electrolytic non-redox system. The electrolytic non-redox (and redox too) systems can be considered according to GATES principles [14], if all

- (i) qualitative (specification of components forming a system, and species in the system thus formed),
- (ii) qualitative (concentration of components), and
- (iii) physicochemical (thermodynamic equilibrium constants) is available. Any non-redox system is formulated with use of charge and concentration balances, and complete set of expressions for equilibrium constants. Charge balance involves charged species of a system.

The set of concentration balances involves relations between concentrations of components and species, formulated – separately – for particular elements or cores $\neq \text{H}, \text{O}$. For a redox system, the set of elemental balances is completed by Generalized Electron Balance (GEB), formulated on the basis of the $2f(\text{O}) - f(\text{H})$ balance [15], within GATES/GEB. Some examples of redox systems were presented also in this Journal [16].

Static and dynamic electrolytic systems are distinguished. A dynamic system is realized in titration, where V mL of titrant T is added into V_0 mL of titrand D, and V_0+V mL of D+T mixture is obtained at defined point of the titration [17]. Concentrations of solutes (a) in D are denoted by C_0 (for analyte), C_{01} , C_{02} , ... and (b) in T by C (for reagent), C_1 , C_2 , In the reference system considered here, $\text{Hg}(\text{NO}_3)_2$ (C) is the reagent, NaCl (C_0) is the analyte, $\text{Na}_2\text{Fe}(\text{CN})_5\text{NO}\cdot 2\text{H}_2\text{O}$ (C_{01}) is the indicator. Moreover, HNO_3 (C_1) is the component in T that prevents precipitation of HgO when $\text{Hg}(\text{NO}_3)_2$ solution is prepared as T.

Within GATES there are considered, among others, the systems in which a solid phase is formed. Examples of this kind are provided e.g. in [6]. There may also be a change in the solid phase composition, see e.g. [18].

The results of calculations performed according to GATES principles with use of iterative computer programs [14], can be presented graphically on the related 2D diagrams, where the fraction titrated

$$\phi = \frac{CV}{C_0V_0} \quad (1)$$

is marked on the abscissa, as an independent variable, where C and C_0 are expressed in mol/L, V and V_0 in mL. This is the simple way to normalize the respective graphs, i.e., the independence of their shape from the V_0 value.

The Φ plays also the key role in formulation of Generalized Equivalence Mass (GEM) concept [19], compatible with GATES principles. Within GEM formulation, the end (e) and equivalence (eq) points are related to the titration curve. At the end point, the visual titration is terminated, when indicated by a desired/pre-assumed color change of the D+T mixture, or by the first appearance of a solid phase, e.g. AgI in the Liebig-Denigès method [6], or $\text{HgFe}(\text{CN})_5\text{NO}$ in the titration considered here. Turbidity in D+T provides the appropriate indicator (indicating component), e.g., KI in the Liebig-Denigès method, or $\text{Na}_2\text{Fe}(\text{CN})_5\text{NO}\cdot 2\text{H}_2\text{O}$ in the method discussed here.

Equation (1) can be rewritten as follows

$$\frac{V}{\phi} = \frac{C_0V_0}{C} \quad (2)$$

As we see, the fraction V/Φ value is constant during the titration in D+T system; it depends only on the pre-assumed/ imposed values for C, C_0 (intensive quantities) and V_0 . From Eq. (2) it follows that V/Φ takes the same value at the end (e) and equivalent (eq) points, i.e.,

$$\frac{V}{\phi} = \left(\frac{V}{\phi}\right)_e = \left(\frac{V}{\phi}\right)_{eq} \Rightarrow \frac{V}{\phi} = \frac{V_e}{\phi_e} = \frac{V_{eq}}{\phi_{eq}} \quad (3)$$

We have

$$C_0V_0 = 10^3 \cdot \frac{m_A}{M_A} \quad (4)$$

where m_A [g] and M_A [g/mol] denote mass and molar mass of the analyte (A), respectively. From Equations (1) and (4) it follows that

$$m_A = 10^{-3} \cdot C \cdot M_A \cdot \frac{V}{\phi} \quad (5)$$

From (3) and (5) one obtains:

$$m_A = 10^{-3} \cdot C \cdot M_A \cdot \frac{V_e}{\phi_e} \quad (5a)$$

$$m_A = 10^{-3} \cdot C \cdot M_A \cdot \frac{V_{eq}}{\phi_{eq}} \quad (5b)$$

However, Eq. (5a) cannot be applied for the evaluation of m_A (V_e known, Φ_e unknown). Also, Eq. (5b) is useless (the "rounded" Φ_{eq} value is known exactly, but V_{eq} is unknown), as V_e (not V_{eq}) in visual titrations is determined experimentally.

Because the Equations (5a) and (5b) are inapplicable, the third, approximate formula for m_A has to be applied, namely:

$$m'_A = 10^{-3} \cdot C \cdot M_A \cdot \frac{V_e}{\phi_{eq}} = 10^{-3} \cdot C \cdot V_e \cdot \frac{M_A}{\phi_{eq}} = 10^{-3} \cdot C \cdot V_e \cdot R_A^{eq} \quad (6)$$

where Φ_{eq} is put for Φ_e in Eq. (5a), and

$$R_A^{eq} = \frac{M_A}{\Phi_{eq}} \quad (7)$$

is named as the equivalent mass of the analyte A. The relative error in accuracy resulting from this substitution equals to

$$g = \frac{m'_A - m_A}{m_A} = \frac{m'_A}{m_A} - 1 = \frac{V_e}{V_{eq}} - 1 = \frac{\phi_e}{\phi_{eq}} - 1 \quad (8)$$

For $\Phi_e = \Phi_{eq}$ one gets $g = 0$ and $m'_A = m_A$; thus $\Phi_e \cong \Phi_{eq}$, i.e. $V_e \cong V_{eq}$ corresponds to $m'_A \cong m_A$.

A conscious choice of an indicator and its color change during the titration is possible on the basis of analysis of the related titration curve. In particular, at $\Phi_{eq} = 1/2$ we have $g = 2\phi_e - 1$. The g values are usually expressed in %.

The numerical values for Φ_e are usually close to Φ_{eq} values expressed by a ratio of small natural numbers [19]. For example, in the system considered here we have $\Phi_{eq} = 1/2$. The difference $\Phi_e - \Phi_{eq}$, when compared with the uncertainty of Φ value, is acceptable from the one-drop error viewpoint when $|\Phi_e - \Phi_{eq}| < 0.003$ [19].

Calculation procedure

The calculation specified below differs significantly from the one usually practiced in GATES, where a complete set of independent balances and equilibrium constants is applied. In particular, the GATES procedure can be applied to the model D+T system with NaCl (C_0) + $\text{Na}_2\text{Fe}(\text{CN})_5\text{NO}\cdot 2\text{H}_2\text{O}$ (C_{01}) as titrand D (V_0), and $\text{Hg}(\text{NO}_3)_2$ (C) + HNO_3 (C_1) as titrant T (V). However, the mercurimetric titration is applied also for the chloride samples from more complex media, where composition of a sample matrix is undefined [20]. Some kinds of the samples were also tested in clinical laboratories, e.g. [21]. Other indicators were also applied for this purpose, see [22].

In the simplified calculation procedure, charge balance and other concentration balances (except for Cl and Hg, and nitroprusside) are omitted. The concentration balances are confined to mono-phase system, including the end (e) point, i.e. the first point of the titration, where the solubility product ($K_{sp} = [\text{Hg}][\text{Fe}(\text{CN})_5\text{NO}]$, $\text{p}K_{sp} = 8.6$) of $\text{HgFe}(\text{CN})_5\text{NO}$ is valid.

From concentration balances for Cl and Hg:

$$[Cl] + \sum_{i=1}^4 [HgCl_i] = \frac{C_0 V_0}{V_0 + V_e} \quad (9)$$

$$[Hg] + \sum_{i=1}^2 [Hg(OH)_i] + \sum_{i=1}^4 [HgCl_i] = \frac{CV}{V_0 + V_e} \quad (10)$$

we have, by turns,

$$F = \frac{\sum_{i=1}^4 i [HgCl_i]}{[Hg] + \sum_{i=1}^2 [Hg(OH)_i] + \sum_{i=1}^4 [HgCl_i]} = \frac{\frac{C_0 V_0}{V_0 + V_e} - [Cl]}{\frac{CV}{V_0 + V_e}} \quad (11)$$

i.e., the fraction titrated (Eq. 1) has the form

$$\phi = \frac{CV}{C_0 V_0} = \frac{C}{C_0} \cdot \frac{C_0 - [Cl]}{C.F + [Cl]} \quad (12)$$

where

$$F = \frac{\sum_{i=1}^4 i K_i^{Cl} [Cl]^i}{1 + \sum_{i=1}^2 K_i^{OH} [OH]^i + \sum_{i=1}^4 K_i^{Cl} [Cl]^i} \quad (13)$$

and $[Hg(OH)_i] = K_i^{OH} [Hg][OH]^i$ ($i=1,2, \log K_i^{OH} = 10.3, 21.7$), $[HgCl_i] = K_i^{Cl} [Hg][Cl]^i$ ($i=1,2,3,4; \log K_i^{Cl} = 6.74, 13.22, 14.07, 15.07$). The $pCl = -\log[Cl]$ vs Φ dependence, obtained from Equations (12) and (13), is considered as titration curve, and presented in Figure 1. It should be noted that the jump on this curve occurs in close vicinity of the fraction titrated value $\Phi = \Phi_{eq} = 1/2$.

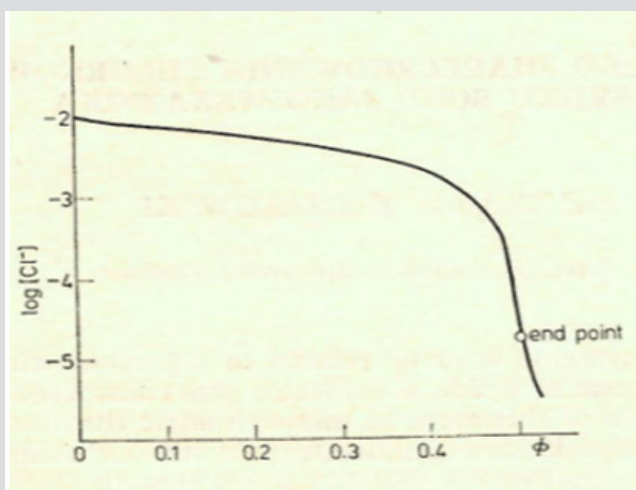


Figure 1: The titration curve for mercurimetric titration of chloride at $C_0 = 0.01$, $C_{01} = 0.003$, $C = 0.1$.

A detailed discussion on the balances (9), (10) leads to conclusion that at the vicinity of the end (e) point, $pCl \approx 4.7$, $[Hg(OH)_2] \ll [HgOH] \ll [Hg] \ll [HgCl] < [HgCl_2] \gg [HgCl_3] \gg [HgCl_4]$, it can be simplified into the form

$$F = \frac{K_1^{Cl} + 2K_2^{Cl} [Cl]}{K_1^{Cl} + K_2^{Cl} [Cl]} \quad (14)$$

Let $V = V_e$ denotes the volume of titrant where the solubility product K_{sp} of $HgFe(CN)_5NO$ is attained. Assuming that nitroprusside ion does not form protonated species [23], at $V = V_e$ we have:

$$[Fe(CN)_5NO] = \frac{C_{01} V_{01}}{(V_0 + V_e)}, [Hg] = \frac{K_{sp}}{C_{01} V_0} \cdot (V_0 + V_e)$$

$$[Hg] (K_1^{Cl} [Cl] + K_2^{Cl} [Cl]^2) = \frac{CV_e}{V_0 + V_e}$$

$$\text{and then } CV_e = \frac{K_{sp}}{C_{01} V_0} \cdot (V_0 + V_e)^2 \cdot (K_1^{Cl} + K_2^{Cl} [Cl]) \cdot [Cl] \quad (15)$$

If $[Cl] \ll C \cdot F$, at $V = V_e$, from Equations (12) and (14) we have

$$CV_e = V_0 \cdot (C_0 - [Cl]) \cdot \frac{K_1^{Cl} + 2K_2^{Cl} [Cl]}{K_1^{Cl} + K_2^{Cl} [Cl]} \quad (16)$$

From Equations (15) and (16) we have the equation

$$2A \cdot [Cl]^2 + B \cdot [Cl] - C_0 V_0 = 0$$

where

$$A = K_2^{Cl} \cdot \frac{K_{sp}}{C_{01} V_0} \cdot (V_0 + V_e)^2, B = K_1^{Cl} \cdot \frac{K_{sp}}{C_{01} V_0} \cdot (V_0 + V_e)^2 + V_0$$

Then we have

$$[Cl] = \frac{\sqrt{\Delta} - B}{4A} = \frac{2C_0 V_0}{\sqrt{\Delta} + B} \quad (17)$$

where

$$\Delta = B^2 + 8A \cdot C_0 V_0$$

Setting (17) into (15) gives the equation

$$\frac{2K_{sp} C_0}{C_{01} C} \cdot (V_0 + V_e)^2 \cdot \left(K_1^{Cl} + 2K_2^{Cl} \cdot \frac{C_0 V_0}{\sqrt{\Delta} + B} \right) \cdot (\sqrt{\Delta} + B)^{-1} - V_e = 0 \quad (18)$$

The V_e value can be found from Equation (18) according to zeroing procedure, realized with use of a computer program for particular $V_0, C, C_0, C_{01}, K_{sp}, K_1^{Cl}$ and K_2^{Cl} values, considered as parameters of this equation. Then the relative systematic error involved with mass of chloride determination will be calculated in accordance with the principles of Generalized Equivalence Mass (GEM) formulation [19,24], and illustrated in Figure 2.

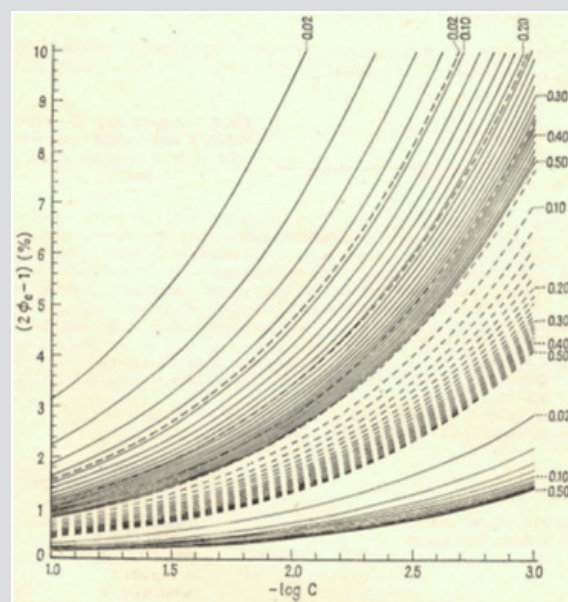


Figure 2: The $2\Phi_e - 1$ (in %) vs. $-\log C$ dependences plotted at different $q = C_0/C$ values; 0.02, 0.04, ..., 0.48, 0.50 at
 a) $C_{01} = 0.01$ (lower continuous lines)
 b) $C_{01} = 0.003$ (dotted lines)
 c) $C_{01} = 0.001$ (upper continuous lines); the numbers on right side and at the top of the figure indicate the corresponding q -values.

Final Comments

The paper provides an example of application of physicochemical (thermodynamic) knowledge involved with gaining the information involved with expected systematic error of analyses made at different concentrations of NaCl (C_0), $\text{Na}_2\text{Fe}(\text{CN})_5\text{NO}\cdot 2\text{H}_2\text{O}$ (C_{01}) and $\text{Hg}(\text{NO}_3)_2$ (C). Generally, at given C value, the error of chloride analysis grows with a decrease of C_0 and C_{01} values, as indicated in Figure 2.

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